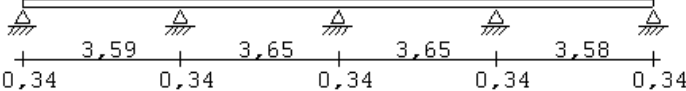


Travi T9 - T10 - T11 - T12

acc. : $f_{yk} = 4500 \text{ daN/cm}^2$	$f_{yd} = f_{yk} / 1,15 = 3913 \text{ daN/cm}^2$	copriferro sup : 3,00 cm
cls. : $R_{ck} = 250 \text{ daN/cm}^2$	$f_{cd} = 0,85 \times f_{ck} / 1,50 = 118 \text{ daN/cm}^2$	copriferro inf : 3,00 cm
Coeff.Car.Perm. Strutturali= 1,30	$E_c = 314470 \text{ daN/cm}^2$	Coeff.Car.Variabili= 1,50
Coeff.Car.Perm. Non Strutt.= 1,50		Coeff.Car.Sismici = 0,30

CARICHI (daN/m)

Q	297	297	297	297
G2	1150	1150	1150	1150
G1	308	307	307	307
p.p.	512	512	512	512
				
f. (l/2) (cm)	-0,059	-0,025	-0,025	-0,058
f.max. (cm)	-0,060	-0,025	-0,025	-0,059
pos. (m)	1,60	1,95	1,70	2,00
f/l	1/5973	1/14600	1/14484	1/6037

DATI GEOMETRICI SEZIONE

asta	luce(m)	B.sup	H.sez.	B.inf	s.anima	s.ala sup.	s.ala inf.	J(cm4)
1 T9	3,59	80	30		45	20		136108 (T)
2 T10	3,65	80	30		45	20		136108 (T)
3 T11	3,65	80	30		45	20		136108 (T)
4 T12	3,58	80	30		45	20		136108 (T)

REAZIONI VERTICALI APPOGGI

nodo	N.max. [daN]	N.perm. [daN]
1 P11	5037	1154
2 P12	14061	3382
3 P13	12871	2801
4 P14	14038	3375
5 P15	5021	1149

Travi T9 - T10 - T11 - T12

MOMENTI MAX. (+) IN CAMPATA

asta	pos. [m]	MEd[daNm]		MRd[daNm]	X[cm]	X/d	arm.inf.[cm ²]	arm.sup.[cm ²]
1	1,55	3918	<	9384	3,64	0,13	(9,55)	7 Ø 12 (7,92)
2	1,90	2976	<	8922	3,54	0,13	8 Ø 12 (9,04)	7 Ø 12 (7,92)
3	1,75	2979	<	8922	3,54	0,13	8 Ø 12 (9,04)	7 Ø 12 (7,92)
4	2,05	3895	<	9384	3,64	0,13	(9,55)	7 Ø 12 (7,92)

MOMENTI MAX. (-) SU APPOGGI

asta	nodo	MEd[daNm]		MRd[daNm]	X[cm]	X/d	arm.sup.[cm ²]	arm.inf.[cm ²]
1	sx. dx.	-4946	<	-15093	4,43	0,16	7 Ø 12 (4,69) 14 Ø 12 (15,84)	(6,74) (18,59)
2	sx. dx.	-4946 -4237	< <	-15093 -15111	4,43 4,48	0,16 0,17	14 Ø 12 (15,84) 14 Ø 12 (15,84)	(18,59) 16 Ø 12 (18,08)
3	sx. dx.	-4237 -4930	< <	-15111 -15093	4,48 4,43	0,17 0,16	14 Ø 12 (15,84) 14 Ø 12 (15,84)	16 Ø 12 (18,08) (18,59)
4	sx. dx.	-4930	<	-15093	4,43	0,16	14 Ø 12 (15,84) 7 Ø 12 (4,85)	(18,59) (6,84)

TAGLIO SLU cdc non Sismica

asta	nodo	VEd[daN]		VRd[daN]	VRd'	VRcd	VRsd	staffe
1	sx. dx.	5037 7188	< <	13656 13656	6827 8590	32144 32144	13656 13656	Ø 8/ 7 cm Ø 8/ 7 cm
2	sx. dx.	6873 6435	< <	13656 13656	8590 8511	32144 32144	13656 13656	Ø 8/ 7 cm Ø 8/ 7 cm
3	sx. dx.	6436 6869	< <	13656 13656	8511 8590	32144 32144	13656 13656	Ø 8/ 7 cm Ø 8/ 7 cm
4	sx. dx.	7169 5021	< <	13656 13656	8590 6880	32144 32144	13656 13656	Ø 8/ 7 cm Ø 8/ 7 cm

VEd
VRd = min (VRcd, VRsd)

Taglio di Calcolo
Taglio Resistente

VRd' = $(0.18 k (100 \text{ ro } f_{ck})^{(1/3)}) / 1,50 \text{ bw } d$
VRmin = $(0.035 k^{(3/2)} f_{ck}^{(1/2)} \text{ bw } d$

Taglio Res.senza staffe k = $1 + (20/d)^{(1/2)} \leq 2$
Taglio Res.Min. VRd' $\geq$ VRmin

VRcd = $0.9 d \text{ bw } f'_{cd} \text{ ctg} \theta / (1 + \text{ctg}^2 \theta)$
VRsd = $0.9 d A_{sw} f_{yd} \text{ ctg} \theta$

Taglio Res.cls compresso f'cd = $0.5 x f_{cd} = 59 \text{ daN/cm}^2$
Taglio Res.con staffe

ctg $\theta = 1,00$

inclinazione biella cls

Travi T9 - T10 - T11 - T12

STATO LIMITE DI TENSIONI DI ESERCIZIO

Grado di aggressività ambientale : ordinarie (a)

Asta	Q.acc.	M[daNm]	$\sigma.f.$ [daN/cm ²]	$\sigma.c.t$ [daN/cm ²]	$\sigma.c.c$ [daN/cm ²]
1	RARA	2312	992		25,49 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	2121	910		23,38 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	2044	877		22,53 < 93,38 = 0,45 fck
2	RARA	1280		12,09	9,98 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	1122		10,60	8,75 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	1059		10,00	8,26 < 93,38 = 0,45 fck
3	RARA	1285		12,13	10,02 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	1127		10,64	8,79 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	1064		10,05	8,30 < 93,38 = 0,45 fck
4	RARA	2300	987		25,35 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	2110	905		23,26 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	2033	872		22,41 < 93,38 = 0,45 fck

Tensione di Trazione CLS : 1.2 fctm 18,88 (sez.non fessurata)

Tensione di Trazione ACC : 0.8 fyk 3600 (sez. fessurata)

Nodo	Q.acc.	M[daNm]	$\sigma.f.$ [daN/cm ²]	$\sigma.c.t$ [daN/cm ²]	$\sigma.c.c$ [daN/cm ²]
1	RARA	0			
	FREQUENTE (0,5)	0			
	QUASI PERM. (0,3)	0			
2	RARA	-3214	851		32,47 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	-2980	789		30,11 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	-2887		18,75	21,92 < 93,38 = 0,45 fck
3	RARA	-2332		15,20	17,86 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	-2121		13,82	16,25 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	-2036		13,27	15,60 < 93,38 = 0,45 fck
4	RARA	-3202	847		32,35 < 124,50 = 0.60 fck
	FREQUENTE (0,5)	-2969	786		30,00 < 93,38 = 0,45 fck
	QUASI PERM. (0,3)	-2876		18,68	21,84 < 93,38 = 0,45 fck
5	RARA	0			
	FREQUENTE (0,5)	0			
	QUASI PERM. (0,3)	0			

Tensione di Trazione CLS : 1.2 fctm 18,88 (sez.non fessurata)

Tensione di Trazione ACC : 0.8 fyk 3600 (sez. fessurata)

Travi T9 - T10 - T11 - T12

STATO LIMITE DI FESSURAZIONE

Grado di aggressività ambientale : Cond.amb. ordinarie

Comb.Carichi : FREQUENTE				Comb.Carichi : QUASI PERMANENTE			
Asta	$E_{xsm} \times S_{rm}$	=	$W_m \times 1,70 = W_k$ (mm)	$E_{xsm} \times S_{rm}$	=	$W_m \times 1,70 = W_k$ (mm)	
1	$0,00043 \times 97,06$	=	$0,04$	$0,00042 \times 97,06$	=	$0,0405$	$0,069 < 0,30$
2	$0,00024 \times 93,19$	=	$0,02$	$0,00023 \times 93,19$	=	$0,0213$	$0,036 < 0,30$
3	$0,00024 \times 93,19$	=	$0,02$	$0,00023 \times 93,19$	=	$0,0214$	$0,036 < 0,30$
4	$0,00043 \times 97,06$	=	$0,04$	$0,00042 \times 97,06$	=	$0,0403$	$0,069 < 0,30$

Comb.Carichi : FREQUENTE				Comb.Carichi : QUASI PERMANENTE			
Nodo	$E_{xsm} \times S_{rm}$	=	$W_m \times 1,70 = W_k$ (mm)	$E_{xsm} \times S_{rm}$	=	$W_m \times 1,70 = W_k$ (mm)	
1							
2	$0,00038 \times 93,93$	=	$0,04$	$0,00036 \times 93,93$	=	$0,0342$	$0,058 < 0,30$
3	$0,00027 \times 93,93$	=	$0,03$	$0,00026 \times 93,93$	=	$0,0241$	$0,041 < 0,30$
4	$0,00037 \times 93,93$	=	$0,04$	$0,00036 \times 93,93$	=	$0,0340$	$0,058 < 0,30$
5							

E_{sm} = deformazione media
 S_{rm} = distanza media tra le fessure (mm)
 $W_m = E_{sm} \times S_{rm}$: valore medio dell'apertura
 $W_k = 1,7 \times W_m$: valore caratteristico apertura